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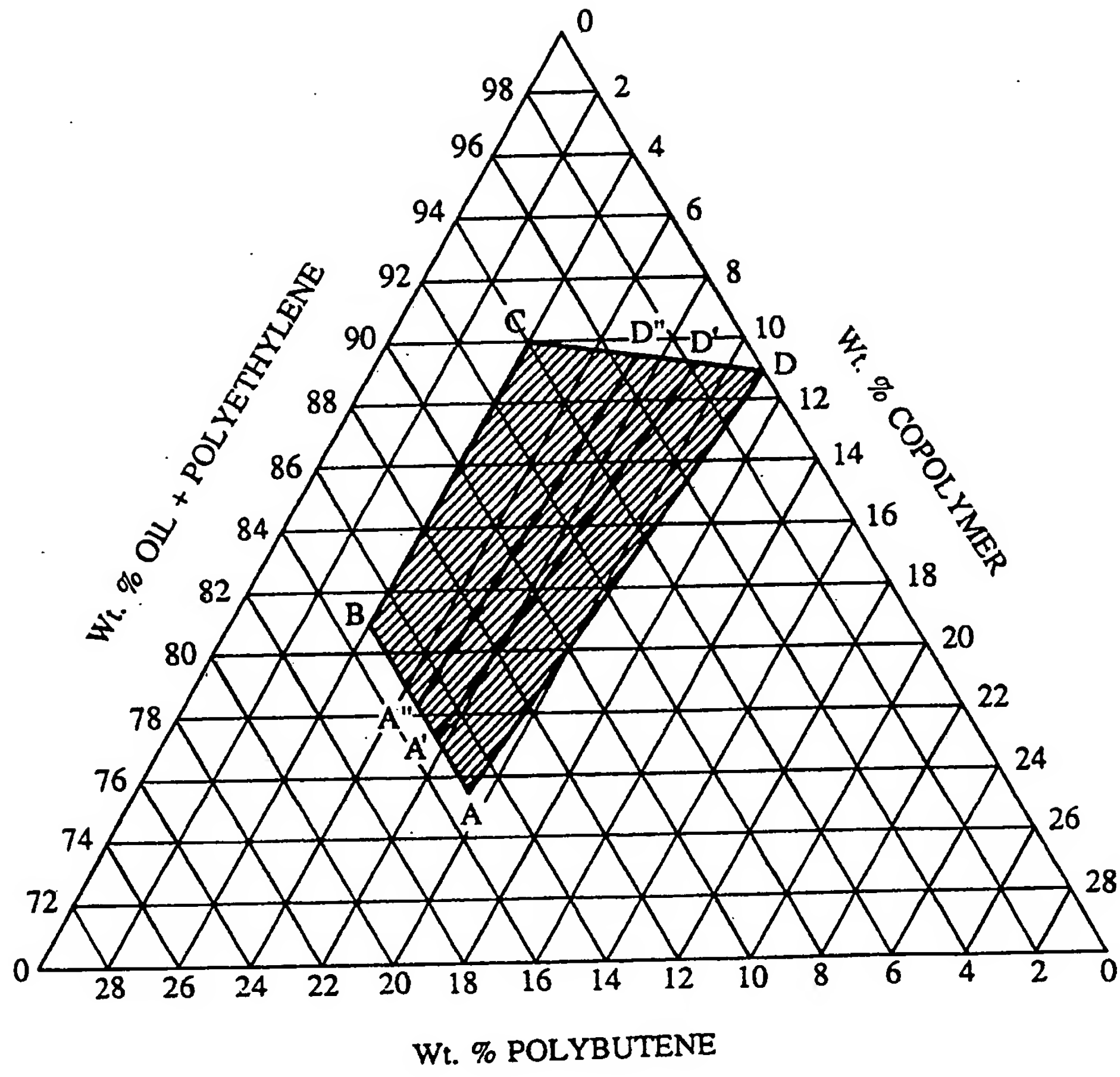
**C3M**

**C3V**

(54) **Filled cables**

(57) A material for filling voids in the waterproof cables comprises a styrene-rubber diblock copolymer, a naphthenic or paraffinic oil and a polyethylene wax. The cables are suitable for aerial as well as underground use.

**GB 2 195 642 A**



## SPECIFICATION

## Filled cables

5 *Technical Field*

This invention relates to cables having a waterproofing filling material therein.

*Background of the Invention*

Cable used in the telecommunications industry, such as in telephone systems, generally requires a waterproofing filling material in the cable to protect the cable from water entry. This is true whether the cable is buried beneath the ground or laid under water. It is also sometimes required in aerial applications.

Attempts to waterproof cable such as buried cable began nearly 100 years ago and were unsuccessful in a practical sense until the introduction of plastic insulated cable during the 1950's. Specially sheathed cables, with dual plastic coatings encasing an aluminum shield, have been used successfully and are still being buried in dry environments. Pressurized cable also contends successfully with water problems. However, both of these approaches are deficient, the former leaves the cable vulnerable and the latter is expensive to maintain. Since 1970, large quantities of cable have been filled with waterproofing compounds. This approach followed the recognition that in plastic insulated cable the localized intrusion of water into the cable sheath is not in itself a serious problem. Disruption of deterioration of service occurs when long lengths of cable become flooded. Flooding occurs because water that penetrates into a localized opening in the cable sheath is free to channel as far as gravity allows, often hundreds of feet. Not only does this upset the capacitance balance of the transmission lines, but it introduces more potential corrosion sites in proportion to the length of wire that is wetted. Corrosion typically occurs slowly, but the useful life of water soaked wires is obviously shorter than that of dry wires.

A solution that has been widely adopted is to fill the voids in the cable with a water insoluble filling material that simply plugs the cable to channeling water. However, though the physical function of the cable filling material is straight forward, the choice of the material is not. Among the many considerations that are important for materials used in this application are the hydrophobic nature of the material, stability on aging, low temperature properties, flow characteristics at elevated temperatures, processing characteristics, handling characteristics, dielectric properties, toxicity and cost.

Materials that satisfy most of these criteria, and which have been used widely in this application, are described in U.S. Patent 3,607,487 and U.S. Patent 3,717,716. These materials are essentially a petroleum jelly mixed with a polymer, usually polyethylene, to impart consistency and prevent flowing at warm temperatures.

Similar hydrophobic filling materials have been proposed for filling splice closures. For example, U.S. Patent 3,879,575 describes a mixture of a low viscosity oil, gelled by a styrene-isoprene-styrene copolymer, again with a polyethylene wax added to impart consistency and reduce slump.

More recently, an improvement over the petroleum jelly-polyethylene wax cable filling material has been disclosed in U.S. Patent 4,259,540. This patent discloses a material which overcomes the objectionable handling characteristics of the petroleum jelly-polyethylene cable filling material. For example, since installation and maintenance of cables often requires the cable to be spliced, such splicing generally requires the isolation and removal of filling material from individual wires or optical fibers in the splice region where the cables are filled with the petroleum jelly material. Otherwise, an oily interface may form between the wire and the polyurethane material subsequently used to encapsulate (waterproof) the splice. This oily interface can serve as a path for water entry into the splice. This results in soiling hands, equipment and clothing. Moreover, removing just sufficient material to effect the splice is time consuming and the task is generally undesirable. Further, handling low temperatures is significantly more difficult, necessitating an occasion, use of a torch to preheat the cable or the use of solvents to soften the encapsulated core. The improved material described in U.S. Patent 4,259,540 overcomes the aforementioned objections to the cable filled with the petroleum jelly-polyethylene material. The improved material according to the patent is a mixture of a naphthenic or paraffinic oil having specific characteristics, a styrene-ethylene butylene-styrene (S-EB-S) triblock copolymer having a styrene-rubber ratio of from about 0.2 to 0.5 and polyethylene having a softening point of 110°C to 130°C. It should be noted that the term styrene-rubber ratio, when used herein, refers to the weight ratio of the styrene block to the rubber block in the copolymer. Further, whenever the term S-EB-S is employed, it refers to a triblock copolymer whereas the term S-EB refers to a diblock copolymer.

While the cable in accordance with U.S. Patent 4,259,540 is excellent for use in underground applications, it has certain shortcomings with respect to use for aerial applications. These

shortcomings are due generally to compound flow-out of the cable especially where solar heating (up to 80°C) is a factor. Also, at elevated temperatures, the mutual capacitance between electrical conductors of a typical copper wire cable increases due to migration of the oil component into the cell structure of the conductor insulation which generally consists of foamed polyethylene. While U.K. Patent Application GB 2 092 176 A teaches that such cell filling can be prevented by the addition of a polybutene oil, and it is generally known that high temperature flow can be attained by increasing the polyethylene wax level present in such compositions, unfortunately, the addition of polybutene oil and an increase in polyethylene wax level both lead to an increase processing viscosity. High viscosity makes it difficult to penetrate and fill the core of large pair count cable. As general rule, filling should be done at no higher than about 110°C to prevent damage of the foamed polyethylene insulation and should have a viscosity of less than about 60 centipoise at that temperature to effect filling of large pair sized cable.

Attempts to lower the viscosity by reducing the rubber content of the S-EB-S copolymer have been unsuccessful because such compounds do not properly gel the oil. That is, a minimum level of S-EB-S, of about 5.5 percent by weight is required. Even at a 5.5 percent by weight S-EB-S level, some slight oil separation (syneresis) is often seen as a result of these problems. In order to control this syneresis, U.S. Patent 4,259,540 teaches that a syneresis inhibitor may be added. Such inhibitors are not necessary with the filling formulations of this invention. Filled cables intended for aerial use have used a blend of petroleum jelly and polyethylene wax. Such cables exhibit the drawbacks of the buried petroleum jelly cables previously discussed.

Applicant has now discovered a filling composition which is a modification of the composition described in U.S. Patent 4,259,540 which is included herein by reference, and which overcomes the problems stated above for aerial use, but yet retains all of the other properties which make the cable suitable for use as buried cable. Consequently, cable using the filling compound as described herein is not only suitable for use as buried cable, but is also suitable for aerial use as well.

#### *Summary of the Invention*

A cable comprises a plurality of strands which may be, for example, insulated electrical wire conductors or optical fiber conductors, contained within a sheath leaving voids between the strands and between the strands and the sheath, and a filling material filling the voids. The invention is characterized in that the filling material comprises a mixture of a styrene-rubber diblock copolymer typically having a styrene/rubber ratio of from about 0.2 to 0.5; an oil such as those defined by ASTM D2226 type 103, 104A, 104B, or mixtures thereof; and polyethylene. Additionally, the filling composition may include a styrene-rubber styrene triblock copolymer and/or a polybutene oil. The amounts of the foregoing ingredients are formulated in proportions to give a cable filling material that meets the functional requirements for the cable employing such material for both buried and aerial use. The material has high temperature flow, capacitance stability and processing characteristics superior to those of prior art material.

#### *Brief Description of the Drawing*

The FIGURE is a ternary compositional diagram setting forth composition ranges of the cable filling material which is employed in the novel cable of the present invention.

#### *Detailed Description*

The cable of the present invention is an improvement over the cable disclosed in U.S. Patent 4,259,540 in that it retains all the positive attributes of the prior art cable and yet in addition, has capacitance stability and high temperature flow resistance which are required for aerial use, and further does not exhibit oil separation. In addition, the filling compound for waterproofing of the novel cable is easily injected into the cable.

The filling compound of the novel cable employs a styrene-rubber diblock copolymer to replace all or part of the styrene-rubber-styrene triblock copolymer cited in the U.S. Patent 4,259,540. Applicant has discovered that the prior art rubber, which is capped on both ends by styrene, has a higher physical crosslink density than the styrene-rubber diblock copolymer used in the filling composition of the present invention wherein the rubber has a styrene cap on the end only. The crosslinks are physical in nature and result from separate styrene and rubber block domains which form due to the inherent incompatibility of the two types of blocks. Since the styrene blocks are rigid below their T<sub>g</sub> of approximately 90°C, they act as physical crosslinks below the styrene T<sub>g</sub> where the styrene block is on both ends of the molecule (triblock). Applicant has discovered that this lower physical crosslink density results in the oil, which is incorporated in the composition, to be more effectively gelled. Accordingly, syneresis (separation) and cell filling are significantly reduced or eliminated. Further, one may select a styrene-rubber diblock copolymer which is approximately half the molecular weight of the prior art styrene-rubber-styrene copolymer, but yet having the same styrene block to rubber block ratio. This results in a lower viscosity material which makes it possible to add polybutene oil and



polyethylene wax to the filling composition to aid in preventing insulation cell filling and in improving high temperature flow characteristics. If sufficient styrene-rubber copolymer is used, no polybutene oil addition is necessary. However, since the copolymer is generally more costly than the polybutene oil, from an economic standpoint, it is desirable to use a combination of the two materials to prevent cell filling. However, for spliced encapsulant compatibility consideration, it is desirable to minimize the polybutene oil level. Hence, depending upon the consideration which is most important to the user, the formulation can be adjusted in various ways. It is apparent that the substitution of the styrene-rubber diblock copolymer for the styrene-rubber-styrene triblock copolymer of the prior art is extremely desirable.

Even low levels of the styrene-rubber diblock copolymer (about 1%) is found to be particularly useful in formulations which require flame retardant properties where syneresis can be a problem.

The improved cable of this invention can generally be described as one comprising a plurality of conductors (electrical or lightguide) contained within a sheath leaving voids between the conductors and/or between the conductors and the sheath, and a filling material filling the voids wherein the filling material comprises a mixture of a styrene-rubber diblock copolymer having a styrene-to-rubber ratio of from about 0.2 to 0.5, a naphthenic or paraffinic oil, and polyethylene. The amounts of the foregoing ingredients are formulated in proportions so as to result in a cable having a filling material that meets the functional requirements previously set forth for both buried and aerial cable. More particularly, the cable will have a temperature flow of at least about 80°C and a capacitance stability of no greater than 5% increase in the mutual capacitance between insulated conductors at elevated temperature and the composition will have a low viscosity for ease in cable filling.

The styrene-rubber diblock copolymer employed in the cable filling composition is preferably a block copolymer wherein the rubber moiety is saturated. A preferred diblock copolymer is a styrene-ethylene butylene copolymer having a styrene to ethylene butylene ratio of from about 0.2 to 0.5 and preferably in the vicinity of about 0.4. Other rubbers can be substituted for the ethylene butylene block of the copolymer, for example, one may employ ethylene propylene.

The preferred naphthenic and paraffinic oils useful in the filling composition are generally described by ASTM specification D2226 as being type 103, 104A, 104B or mixtures thereof. These preferred oils typically have a minimum specific gravity of 0.85, a minimum SUS viscosity at 210°F of 40 as determined in accordance with ASTM specification D2161 and a maximum pour point as per ASTM D97 of 20°F.

The polyethylene which is included in the formulation of the filling material typically has a softening point of 105°C to 130°C per ASTM E28.

In addition to the above components, the composition may include a styrene-rubber-styrene triblock copolymer such as a styrene-ethylene butylene-styrene copolymer having a styrene-to-rubber ratio of approximately 0.2 to 0.5 and preferably about 0.4 or other styrene-rubber-styrene copolymers wherein the rubber may be, for example, an ethylene propylene. It should be noted that the styrene in any of the aforementioned diblock copolymers includes substituted styrenes. Other additives which may be included in the formulation are polybutene oils or the like.

Various oil polymer mixtures were formulated to arriving at the ingredients described above and the preferred proportions. The preferred proportions for a formulation wherein the styrene-rubber component is a styrene-ethylene butylene diblock copolymer are indicated in the shaded area bounded by lines A, B, C, and D of the FIGURE. The lines AB, A'B, and A''B represent bounds set by encapsulant compatibility. By encapsulant compatibility, it is meant that there is no oil separation at the encapsulant wire interface. This shows a maximum amount of polybutene in the formulation of 15 weight percent. The particular polybutene oil represented in the FIGURE had a molecular weight of 1290. However, polybutene oils of other molecular weights are suitable. The preferred molecular weight range for the polybutene oil is from about 300 to 2,000. The line, BC, represents the minimum amount of the styrene-rubber needed to properly gel the structure and control oil syneresis. As can be seen, this minimum amount of styrene-rubber diblock copolymer is 4 weight percent. The lines CD, CD' and CD'' represent the boundary for mutual capacitance stability, that is, a capacitance which does not vary in an amount of greater than 5%. Further, lines AD, A'D' and A''D'' are the bounds for maximum preferred viscosity of about 60 centipoise. Variation of the ratio of styrene-ethylene butylene diblock copolymer to styrene-ethylene butylene-styrene triblock copolymer will change the area bounded such as by moving from AD to A''D''. Similarly, a change in the molecular weight of any of the components and the type of oil or melting point of the wax may also shift these bounds. Hence, FIGURE depicts the preferred compositional ranges for the particular combination of materials as set forth with respect to the FIGURE. However, these ranges are generally typical to those one would expect even when substituting other suitable polymers or components. Further, the area bounded by lines A, B, C, and D gives the compositional ranges when the rubber portion of the composition is all styrene-ethylene butylene diblock copolymer. When the rubber portion is a

70/30 weight ratio of S-EB/S-EB-S, the preferred range is given by area bounded by A'BCD'. Also, when the rubber is a 40/60 ratio of S-EB/S-EB-S the preferred composition of the filler material for the cable is given by A'BCD'. In all of these compositions, polyethylene wax comprises from 6-7% of the composition. However, a range of about 4-12% of polyethylene wax is useful. This extended range of polyethylene will cause some shifting of the boundaries depicted in the FIGURE. The shift will be a shift of the AD line of the FIGURE whereby lower amounts of polyethylene will lower the AD line to give a broader range and vice versa. Some of the test data used to arrive at the preferred compositional formulations is given in the following Table.

10	TABLE		10
	Constituents	Description	
	A	Styrene-ethylene butylene-styrene triblock copolymer (S-EB-S) having the following properties: styrene/rubber ratio 0.4; sp. gr. 0.91; percent elongation 500; 300 percent modulus ASTM (D412) 700-800 psi; 25°C viscosity, 20 percent in toluene, 400-525 cps (Brookfield Model D RVT, No. 21 spindle). Available from Shell Chemical Co. under the trade designation Kraton G 1652.	5
15			15
20	B	Styrene-ethylene butylene diblock copolymer (S-EB) having a styrene/rubber ratio of 0.4; sp. gr. 0.91; approximately one half the molecular weight of the above-mentioned Kraton G 1652 molecule. Available from Shell Chemical Co. under the designation TRW-7-1511.	20
25			25
	C	A 30/70 by weight ratio of constituents A and B, having a percent elongation of 200 and a 20°C viscosity, 25 percent by weight in toluene of approximately 200 centipoise. Available from Shell Chemical Co. under the trade designation Kraton G 1726X.	30
30			30
	D	Paraffinic based processing oil, type 104B per ASTM D2226, having a pour point per ASTM D97 of 0°F; SUS viscosity at 210°F of 47; sp. gr. 0.86. Available from Sun Chemical Co. under the trade designation Sunpar LW 120.	35
35			35
	E	Polyethylene wax having a softening point per ASTM E28 of 117°F; a hardness per ASTM D5 of 0.5 dmm; density per ASTM D1505 of 0.94; viscosity at 140°C of 400-500 centipoise. Available from Allied Chemical Co. under trade designation AC9.	40
40			40
	F	Polybutene oil having a viscosity of 99°C per ASTM D445 of 635-690 cSt; a pour point per ASTM 97 of +35°F; and average molecular weight of 1290. Available from Amoco Chemical Co. under trade designation Indopol H300.	45
45			45

Example No.	Composition parts by weight	Visco- sity at 110°C cps	Min. slump temp. °C	Capaci- tance change %	Encapsulant pull-out force, lbs.			
					Cable	Hand Dip		
5	1	A-5.5 E-5 D-89 0.5 isopropyl phenyl-phenylphthalate	35	70	13	12	12	5
10	2	C-5.5 E-8 D-86.5	26	≥85	-	-	-	10
15	3	A-4 B-11 D-85	-	-	2.7	-	-	15
20	4	A-2.7 C-4.3 E-5 D-88	38	75	9.4	-	-	20
25	5	C-4.5 E-7 F-15 D-73.5	33	≥85	2.5	-	-	25
30	6	C-5.5 E-7 F-15 D-72.5	39	85	-	-	-	30
35	7	C-4.5 E-7 F-10 D-78.5	28	85	3	-	-	35
40	8	A-1 C-4 E-7 F-10 D-78	34	85	2.7	10	6.5	40
45	9	B-11 E-7 D-82	60	-	-	-	-	45
50	10	A-1.5 C-4 E-6.5 F-4 D-84	32	-	6.8	-	-	50
55	11	A-1.5 C-4 E-6.5 F-7 D-81	35	85	4.6	-	10	55

All of the compositions shown also contain 0.2 parts by weight of an antioxidant such as Irganox 1010 or Irganox 1035 marketed by Ciba-Geigy Corp.

The various compositions were evaluated in terms of five major considerations. These are viscosity, resistance to high temperature flow (slump), capacitance stability, compatibility with urethane type encapsulants and low temperature penetration.

The viscosity measurement indicates the processability of the material. Cables are filled by injecting the filling material into the voids between the wire pairs. Typically, in copper wire cable, this is done after forming a unit of wires or on cable cores consisting of a number of units. Therefore, it is important that the material have a proper viscosity. The filling process involves elevated temperature. From the standpoint of the processing equipment and the effectiveness of the filling process it is more desirable to lower the viscosity of the filling material than to raise the temperature. The operating temperature is limited to the vicinity of 110°C by the insulation commonly used. Therefore, further variation is obtained by choice of the composition. A maximum of 60 centipoise at 110°C has been imposed on the composition for acceptable processing.

The second criteria appearing in the Table is the slump characteristics after two hours exposure to elevated temperatures. This is a measure of the ability of the filling material to retain an acceptably rigid state at elevated service temperatures. Mechanical data is also presented for some examples. A minimum temperature of 80°C has been imposed on the cable for slump.

The test for capacitance stability involves immersion into a beaker of filling compound of a twisted pair of 22 gauge copper wire having insulation thereover consisting of an inner layer of foamed polyethylene and an outer skin of unfoamed polyethylene. This test set-up is heated to 60°C in an oven and the capacitance between wires in the pair and capacitance to ground are monitored as a function of time. Passage of the test requires a maximum increase in the average of the two measurements of not greater than 5% at 100 days exposure. One hundred days at 60°C has been found to correspond to approximately 20 years exposure of aerial cable installed in the Arizona desert.

For the encapsulant compatibility test, insulated conductors having a layer of filled compound are potted in a test fixture with a urethane encapsulant used to fill splice cases. Two thicknesses of filling compound are tested; one characteristic of wire removed from cable and a second thicker layer obtained by a hand dip of the wire in 110°C filling compound. The force required to remove the wire from the test fixture is then measured. The greater the pull-out force, the better the barrier to water penetration at the wire/encapsulant interface. Passage of this test requires a value of a minimum of a four pound pull-out force on wires removed from cable.

Low temperature penetration is measured at 72°F and 0°F using ASTM D937. Passage requires performance comparable to the prior art materials. Typical values for both prior art formulations (U.S. Patent 4,259,540) and formulations in accordance with this invention are 130–150 dmm at 72°F and 80–90 at 0°F. As a point of reference, a polyethylene/petroleum jelly blend used in aerial cable was measured as having a penetration of 19 dmm at 0°F. the lower the penetration number the greater the stiffness of the material.

Although this description deals with primarily electrical cables, it is evident to those skilled in the art that it is equally applicable to cables containing light conductors.

For comparison purposes, Example 1 of the Table, is a filling composition for a cable in accordance with the prior art (U.S. Patent 4,259,540) wherein the rubber material is a styrene-ethylene butylene-styrene triblock copolymer and the filling composition contains no styrene-ethylene butylene diblock copolymer. It can be seen that the capacitance change is significantly higher than the 5% maximum allowed as the standard and further that the slump temperature is well below the 80° minimum temperature set for the slump.

## CLAIMS

1. A cable comprising a plurality of conductors contained within a sheath leaving voids between the conductors and/or between the conductors and the sheath, and a filling material filling the voids, the filling material comprising a mixture of a styrene-rubber diblock copolymer, a compatible oil and polyethylene in proportions to give a cable filling material having a viscosity which facilitates ease in cable filling and wherein the cable has a mutual capacitance stability of no greater than 5% increase in capacitance.

2. A cable as claimed in claim 1, wherein the styrene-rubber diblock copolymer has a styrene/rubber ratio of from about 0.2 to 0.5, and the oil is at least one oil, selected from those oils falling within ASTM D2226, types 103, 104A and 104B.

3. A cable as claimed in claim 1, wherein the oil is selected from the group consisting of naphthenic oils, paraffinic oils and mixtures thereof, and the cable filling material has a minimum flow temperature of about 80°C.

4. A cable as claimed in claim 1, wherein the styrene-rubber diblock copolymer has a styrene/rubber ratio of from about 0.2 to 0.5, and the oil is at least one oil selected from the



group consisting of naphthenic oils and paraffinic oils falling within ASTM D2226 types 103, 104A and 104B.

5. A cable as claimed in claim 4, wherein the styrene-rubber diblock copolymer is a styrene-ethylene butylene diblock copolymer.

- 5 6. A cable as claimed in claim 5, wherein the oil has a minimum specific gravity of about 0.85, a minimum SUS viscosity at 210°F of about 40, and a maximum pour point of about 20°F; and the polyethylene has a softening point of from 105°C to 130°C. 5

- 10 7. A cable filling material for filling voids between conductors and/or between conductors and a sheath of a cable, the material comprising a mixture of a styrene-rubber diblock copolymer, a compatible oil and polyethylene in proportions to give a cable filling material having a viscosity which facilitates ease in cable filling. 10

8. A material as claimed in claim 7 wherein the styrene-rubber diblock copolymer has a styrene/rubber ratio of from about 0.2 to 0.5, and the oil is at least one oil, selected from those oils falling within ASTM D2226, types 103, 104A and 104B.

- 15 9. A material as claimed in claim 7 wherein the oil is selected from the group consisting of naphthenic oils, paraffinic oils and mixtures thereof, and the material has a minimum flow temperature of about 80°C. 15

- 20 10. A material as claimed in claim 7 wherein the styrene-rubber diblock copolymer has a styrene/rubber ratio of from about 0.2 to 0.5, and the oil is at least one oil selected from the group consisting of naphthenic oils and paraffinic oils falling within ASTM D2226 types 103, 104A and 104B. 20

11. A material as claimed in claim 10 wherein the styrene-rubber diblock copolymer is a styrene-ethylene butylene diblock copolymer.

- 25 12. A material as claimed in claim 11, wherein the oil has a minimum specific gravity of about 0.85, a minimum SUS viscosity at 210°F of about 40, and a maximum pour point of about 20°F; and the polyethylene has a softening point of from 105°C to 130°C. 25

13. A cable substantially as herein described with reference to the accompanying drawing.

14. A cable filling material substantially as herein described with reference to the accompanying drawing.

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B5B 35Y 361 369 401 901 902 AA

(56) Documents cited

None

(58) Field of search

B5B

Selected US specifications from IPC sub-class D01F

(54) **Filamentary yarn and film of an aromatic polyetherketone**

(57) A process of melt spinning a yarn or of extruding a film from an aromatic polyetherketone in which prior to spinning or extruding, there is admixed with the polyetherketone polymer in excess of 2% by weight of a plasticiser which is thermally stable at the temperature of the melt and provides a melt of reduced viscosity such plasticiser having volatility characteristics such that though some of the plasticiser volatilises from the spun yarn or extruded film during the process, more than 1% by weight of the plasticiser remains in the spun yarn or extruded film.

GB 2 180 790 A

## SPECIFICATION

## Filamentary yarn and film of an aromatic polyetherketone

- 5 This invention relates to the melt spinning of mono- and multi-filament yarns and to the extrusion of a film from an aromatic polyetherketone and more particularly an aromatic polyetheretherketone. 5

We have found it possible to produce extruded products, more particularly melt spun textile filaments, of an aromatic polyetherketone and more particularly an aromatic polyetheretherketone by conventional melt spinning techniques. This involves melting either a powder or granules of the polymer at between 350°C and 400°C and, using a metering screw or pump, passing the melt to a filter pack where the melt is filtered through graded sand, graded gauzes or sintered metal having a pore size down to about 25 microns. The molten polymer is then extruded through a spinneret at 370°C to 400°C into filaments which are drawn down in a controlled cooling environment. Subsequent processing may involve a reheating of the filaments above 150°C and the drawing of the filaments by a factor of about 3 to complete orientation of the filaments. Film can be produced in a similar manner using a slot die rather than a spinneret. 10 15

However with such techniques we have found it becomes increasingly difficult to produce filaments below 100 microns and more particularly below 50 microns. In the production of filaments 'raining' from the spinneret occurs causing very short lengths of increased diameter to occur in the spun filaments at draw down and it is suspected that the breaks which occur both in the extrusion draw down and in the orientation zone are associated with these discontinuities. This, we have found, limits the fineness of the filaments of polyetheretherketone that can be produced to between 50 and 100 microns depending on the effectiveness of the filtration used. 20 25

In the production of thin films using a slot die instability of the melt curtain edge occurs at thicknesses of about 20 microns and below.

In European Patent Application No 83304022.3 there is described a process of producing a fibre-reinforced composition comprising passing a plurality of continuous filaments of, for example, glass or carbon, through a melt comprising a mixture of a thermoplastic polymer, such as an aromatic polyetheretherketone, and a plasticiser which is thermally stable at least up to the temperature of the melt and having volatility characteristics such that the plasticiser can be volatilised from the composition below the decomposition temperature of the thermoplastic polymer but has sufficiently low volatility at the temperature of the melt to plasticise the polymer and provide a melt of reduced viscosity compared with the melt viscosity of the polymer alone. 30 35

We have now found that the addition of substantial quantities of a plasticiser as used in the process described in European Patent Application No 83304022.3 to a polyetherketone and more particularly a polyetheretherketone before it is melt spun gives rise to a very much more regular extrusion for otherwise similar processing conditions. In addition work done by the extruder screw is reduced considerably and it is possible to reduce the extruder temperature. Consequently we have found using the modified process that filament diameters in the range 20 to 50 microns can be produced without frequent filament breaks. 40

According to the invention, therefore, we provide a process of melt spinning a mono- or multi-filament yarn or of extruding a film from an aromatic polyetherketone and more particularly an aromatic polyetheretherketone in which, prior to spinning or extruding, there is admixed with the polyetherketone polymer a substantial proportion of a plasticiser which is thermally stable at the temperature of the melt and provides a melt of reduced viscosity compared with the melt viscosity of the polymer alone such plasticiser having volatility characteristics such that though some of the plasticiser volatilises from the spun yarn or extruded film during the process, more than 1% by weight of the plasticiser remains in the spun yarn or extruded film. 45

It will be realised, therefore, that in the process all of the plasticiser is not removed the yarn or film and indeed, for certain applications, there are advantages to be gained from this. 50

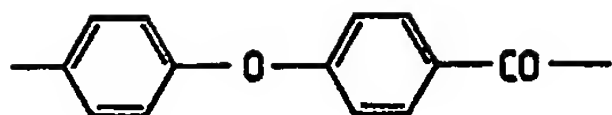
We also provide a melt spun mono- or multi-filament yarn or an extruded film of an aromatic polyetherketone and more particularly an aromatic polyetheretherketone containing in excess of 1% by weight of a plasticiser having the above defined stability and volatility characteristics. 55

Such a yarn or film can be readily converted into a porous yarn or film by an elevated heat treatment process between 250°C and 300°C preferably under vacuum.

According to another aspect of the invention, therefore, we provide a porous yarn or film of an aromatic polyetherketone and more particularly an aromatic polyetheretherketone.

By the term "substantial" which is used in connection with the proportion of plasticiser which is admixed with the polyetheretherketone polymer we mean that in the melt prior to spinning or extruding there is present in excess of 2% by weight of the plasticiser. 60

Suitable polyetherketones for use in the invention include those which contain the recurring unit (I):



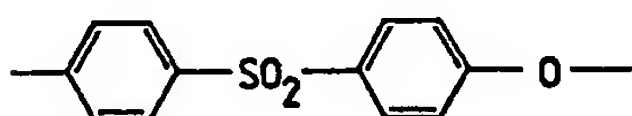
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Such polymers are disclosed, inter alia, in British patent specification 1 414 421 which describes such polymers containing the unit (I) as the sole repeating unit or in conjunction with the repeating unit (II):

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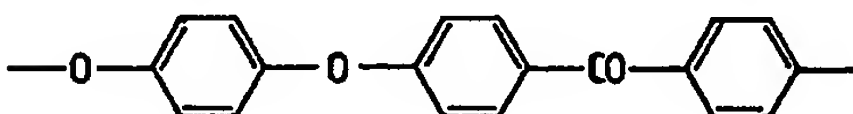
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A preferred polyetheretherketone having the repeating unit (III):

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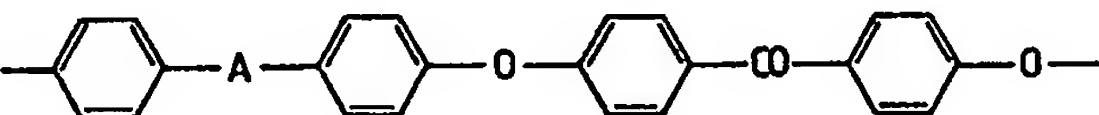


either alone or in conjunction with other repeating units is disclosed in European patent publication No 1879. The other repeating units present in the polymers described in the European application may be of the repeating unit (IV):

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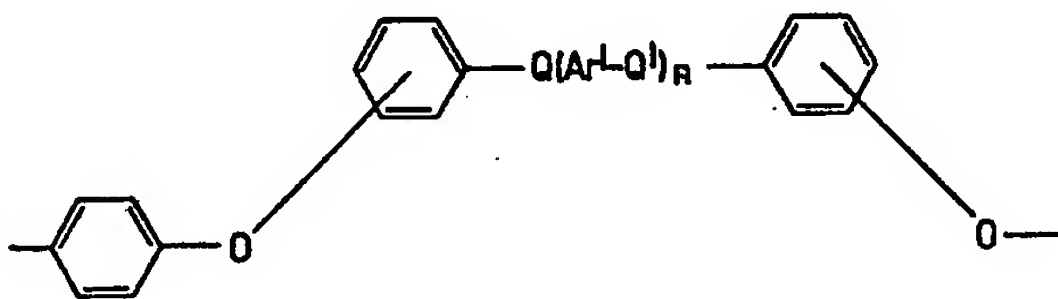
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where A is a direct link, oxygen, sulphur,  $-\text{SO}_2-$ ,  $-\text{CO}-$  or a divalent hydrocarbon radical. The repeat units may also be of formula (V):

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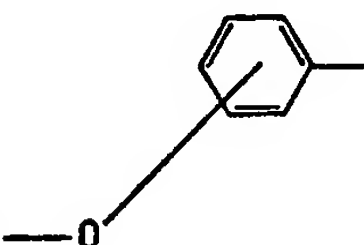
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where the oxygen atom in the sub-units:

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are *ortho* or *para* to the groups Q and Q', Q and Q' which may be the same or different are  $-\text{CO}-$  or  $-\text{SO}_2-$ , Ar' is a divalent aromatic radical, and n is 0, 1, 2 or 3.

The plasticisers which are suitable for use in the invention are materials which are thermally stable at the melt temperatures of polyetheretherketone and which can be partially volatilised from yarns or films during the production thereof in accordance with the invention process. Apart from that the plasticisers used will essentially have the capability of providing a plasticised polymer melt of lower melt viscosity than the polymer itself. Suitable plasticisers having these characteristics are found in the classes aromatic ketones, aromatic sulphones and aromatic esters. Typical plasticisers in these classes are diphenyl sulphone, ditolyl sulphone, benzophenone, phenyl benzoate and benzyl benzoate.

The plasticiser and polymer may be admixed by any conventional technique. For example, a mixture may be achieved:— by dry blending the polymer and the plasticiser, by compounding in a screw extruder, by coating granules of the polymer with a solution of the plasticiser and volatilising the solvent from the coated granules or in suitable cases by adding the plasticiser in the course of producing the polymer.

As mentioned above the mixture of the plasticiser and the polymer will have a reduced melt viscosity compared with the melt viscosity of the polymer alone. Furthermore we have found that the addition of the defined plasticiser serves to greatly reduce the tendency of the melt to

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gel and this contributes to improved processing particularly with a low decitex per filament yarn.

It will of course, be realised that the properties of yarns produced according to the invention will be influenced by the fairly high residual level of plasticiser present. Though the presence of the plasticiser in the filaments of the yarn will detract from their fibre strength, we believe that where the filaments are to be used in a composite yarn structure with, for example, carbon fibre this could offer advantages by reducing the density of the polymer forming the filaments and also by promoting the wetting out of the carbon fibres. We also believe that multifilament yarns produced by the process of the invention would find application in fabrics for special industrial end uses.

- 10 Polyetherketone films produced by the process of the invention include any film produced by a melt extrusion process and may be in substantially amorphous form or may be in molecularly oriented form, such as that resulting from drawing a substantially amorphous film of the polyetherketone. A substantially amorphous film may be achieved by quenching a film produced by melt extrusion on to a cold casting drum. The film may be drawn uniaxially or biaxially. Normally the sheet, if drawn, will be drawn in two directions, the first direction being the direction of extrusion (sometimes termed the 'machine direction' (MD)), the second direction being transverse to the machine direction (sometimes termed 'transverse direction' (TD)). Details of preferred processes for forming oriented films of polyetherketones are disclosed in Research Disclosure 21601, April 1982.
- 20 Typical conditions for the production of a substantially amorphous film by the process of the invention include the extrusion of a molten mixture of the polyetherketone and a melt plasticiser as specified through a slot die with take up of the film on a cooling drum maintained at a nominal temperature of 35°C. The quenched substantially amorphous film may then be subjected to uniaxial or biaxial stretching procedures whilst the film is maintained at a temperature above the second order transition temperature (T<sub>g</sub>) of the polyetherketone. In the case of a polyetherketone of repeat unit -O-Ph-O-Ph-CO-Ph- (Ph is p-phenylene) (available from Imperial Chemical Industries as 'Victrex' PEEK) the drawing, if performed, should be conducted at a temperature of between 140° to 200°C. If a temperature in excess of 200°C is used the film tends to crystallise prematurely giving rise to unacceptable films.
- 30 The drawn films of the invention may be heat set, that is caused to crystallise whilst being restrained from shrinking. For 'Victrex' PEEK appropriate temperatures for the heat step process are in the range 200°C to 320°C.

The main advantage of the present process over that disclosed in Research Disclosure 21601, April 1982 is the co-melt of polyetherketone and plasticiser has viscosity characteristics which are significantly different from those of the melt of the polymer alone and this enables film of much improved quality to be obtained. Additionally the co-melt may be fabricated at lower temperatures than that of the melt alone with consequential benefits. The advantageous viscosity characteristics of the co-melt and the fact that much of the plasticiser can be removed from the film after extrusion offer the benefit of being able to obtain thinner films by the process of the invention.

The films of the invention will inevitably contain plasticiser as they emerge from the extrusion die and provision for removing the plasticiser to an extent consistent with the final application of the film is required. The most convenient means for removing plasticiser makes use of the volatility of the plasticiser employed at temperatures below the decomposition of the polymer. Volatilisation or partial volatilisation of plasticiser may be effected after the co-melt emerges from the die and before it is quenched, by maintaining its temperature above the volatilisation temperature of the plasticiser for a sufficient time to allow for volatilisation of the plasticiser.

Alternatively, removal may be effected by heat treatments which occur as a part of the drawing and heat setting procedure or in additional heat treatment steps. For some applications if may be necessary to provide additional treatments such as solvent extraction, particularly where it is required that the plasticiser content should be less than 1% by weight of the film.

#### EXAMPLE

Process A was carried out on conventional spin-draw equipment with the object of producing 65 f9 multifilament yarn from polyetheretherketone polymer ('Victrex' (Registered Trade Mark) polyetheretherketone polymer, 150P grade, obtainable from Imperial Chemical Industries PLC.

The process used was a conventional one for spinning a low dpf yarn from a thermoplastic polymer (see conditions below). There was considerable 'raining' evident from the spinneret—at least one slub per filament per metre was perceived just below the spinneret. Furthermore the process was unstable with frequent threadline breaks occurring (at least one per minute) in the extrusion and draw zones.

Process B was carried out in a similar manner to Process A except that 30 parts of powdered diphenyl Sulphone was mixed with 70 parts of the same polyetheretherketone polymer prior to drying and feeding to the machine hopper (in the manner of Process A).

65 The main advantages achieved with Process B compared with Process A was the elimination

of 'raining' from the spinneret and a dramatic improvement in the threadline interruption rate so that a practical process performance was achieved. In addition the power requirements of the screw dropped and it was also possible to drop the extrusion temperature to 340°C which is well below that possible for any conventional processing of polyetheretherketone.

5 The processing conditions for Process A and Process B are listed below. 5

	<i>Process A</i>	<i>Process B</i>	
	Screw Speed	2.0 rpm	
	Screw Current	1.5 amps	
10	Melt Temperature	320–380°C	10
	Extrusion Temperature	380°C	
	Pack Filtration	2×200 mesh screens	
	Spinneret	9 hole 0.64 mm dia	
	Feed Roll Speed	32 mpm	
15	Feed Roll Temperature	150°C	15
	Draw Roll Speed	90 mpm	
	Decitex	65 f9	
	% Diphenyl Sulphone in Fibre	0.01%	

## 20 CLAIMS 20

1. A process of melt spinning a mono- or multi-filament yarn or of extruding a film from an aromatic polyetherketone in which, prior to spinning or extruding, there is admixed with the polyetherketone polymer a substantial proportion of a plasticiser which is thermally stable at the temperature of the melt and provides a melt of reduced viscosity compared with the melt viscosity of the polymer alone such plasticiser having volatility characteristics such that though 25 some of the plasticiser volatilises from the spun yarn or extruded film during the process, more than 1% by weight of the plasticiser remains in the spun yarn or extruded film. 25

2. A process as claimed in Claim 1 in which the aromatic polyetherketone is an aromatic polyetheretherketone.

30 3. A process as claimed in either Claim 1 or Claim 2 in which the plasticiser is diphenyl sulphone. 30

4. A melt spun mono- or multi-filament yarn or an extruded film of an aromatic polyetherketone produced by the process of Claim 1 or Claim 3.

5. A melt spun mono- or multi-filament yarn or an extruded film of an aromatic polyetheretherketone produced by the process of Claim 2 or Claim 3. 35

6. A porous yarn or film produced by subjecting the yarn or film as claimed in either Claim 4 or Claim 5 to a heat treatment process.